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# New method of digital modulative adaptative auto-calibration of infrared imaging devices

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#### Abstract

This paper describes the new method of digital auto-calibration IR imaging systems based on using low-amplitude 2D cyclic scanning and solving multi-dimensional inverse problem. The method does not require the use of reference bodies and stages of registration and calibration can coincide. Mathematical algorithms require  $\approx 100~N^2$  operations and are realized by using IBM PC/AT for N < 256.

### 1. Introduction

Modern technology allows to develop IR imaging systems with noise equivalent temperature difference (NETD) of about 0.001 K [1] but the practical realization of these systems and their metrology encounters some problems [2 to 4]. Non-uniformity of IR registrating device is one of these problems to be discussed in the present paper.

Non-uniform sensitivity of IR camera can be due to non-identical elements in the arrays, optical distortions and background irradiation. Digital correction of these effects is possible if the relationships between IR radiation intensity  $l_{i,j}$  and output electrical signals  $a_{i,j}$  are known. In linear approximation:

$$a_{i,j} = g_{i,j} \cdot l_{i,j} + h_{i,j}$$
  $1 \le i,j \le N$  (1)

where N is the number of pixels per line or column.

Coefficients  $g_{i,j}$  and  $h_{i,j}$  are usually determined by use of calibration procedure with two reference bodies, having intensities I1 and I2. Unfortunately, for systems with wide spectral and dynamic range and NETD < 0.1 K, this procedure has some drawbacks.

The best IR arrays use the InSb and CdHgTe detectors [5 and 6] but the attempts to enhance their uniformity, stability and sensitivity up to theoretical limits have still been unsuccessful. Better results were obtained on the base of Simade Schottky diodes arrays [7]. In general, they provide worse than InSb detectors sensitivity but much better uniformity and lack of low-frequency noise [8 and 9]. But even in this case the random variations of spectral sensitivity from one detector to another will limit the temperature resolution of IR systems [10].

It is important that such a problem arises even for single — or few — detectors arrays, for example when high metrological accuracy is needed.

We suggest the new method of adaptive auto-calibration which uses the ideas of modulative spectroscopy [11] and methods of solution for non-correct multi-dimensional inverse problems [12]. The method does not require the use of reference bodies and the stages of registration and calibration can coincide.

## 2. Discussion of inverse problem

The basic idea is to use the low-amplitude two-dimensional (2D) cyclic scanning of the IR camera itself or view angle scanning with additional mirror mounted on the camera. This idea is not new for image processing [13] but the basic problem is choosing of scanning law as simple as possible which permit from minimum number of images to determine correctly all  $g_{i,j}$ ,  $h_{i,j}$  and  $l_{i,j}$  without any essential assumptions about its space characteristics.

The working analog of such a system with  $N \approx 10^4$  is probably the human's eye. During observing the eye do many moves and fast low-amplitude 2D scanning with frequency  $\approx 30\text{-}60$  Hz (tremor) is one of them [14]. Researches in this field last more than fifty years [14 to 16] but the role of tremor in visual information processing is not clear still.

As the basis we have used the simplest 2D cyclic discrete scanning consisting of 3 points. Each pixel is moving for one pixel up or down and one pixel left or right. For this scanning consequence of 3 basic images:

$$\{a_{i,j}\}, \{b_{i,j}\}, \{c_{i,j}\}$$
 (2)

minimum necessary for further processing can be obtained. Unfortunately, restoration of full input information  $\{l_{i,j}\}$  is possible if at least one matrix of coefficients  $\{g_{i,j}\}$ ,  $\{h_{i,j}\}$  is known or has small dispersion. In a case of essential dispersion of both matrices, it is necessary to make two measurements of an object under the following condition:

$$I1 < I2 \tag{3}$$

For absolute and independent calibration of IR system it is enough to place two small-size reference emitters with different /1 and /2 into the frame.

## 3. Equations system and algorithms

According to (1-3) and scanning law an initial system of equations for  $4 N^2 + 4 N$  unknown quantities  $g_{i,j}$ ,  $h_{i,j}$ ,  $l1_{i,j}$  and  $l2_{i,j}$  can be written as following:

$$g_{i,j}.IK_{i,j} + h_{i,j} = aK_{i,j} K = 1,2$$

$$g_{i,j}.IK_{i+1,j} + h_{i,j} = bK_{i,j} 1 \le i,j \le N (4)$$

$$g_{i,j}.IK_{i,j+1} + h_{i,j} = cK_{i,j} g_{1,1} = G^{-1} , h_{1,1} = G^{-1}.H$$

where constants G > 0 and H are determined by the scale of  $I_{i,j}$ .

For correction of non-uniformity it is enough to suppose G=1, H=0. It is important that the structure of system (4) permits to split procedures of restoration  $\{g_{i,j}\}$ ,  $\{h_{i,j}\}$ ,  $\{h_{i,j}\}$ , and  $\{l_{i,j}\}$ .

After subtraction of equations (4) with K=1 from ones with K=2 and elimination of terms  $I2_{i,j} - I1_{i,j}$ , the system for  $g_{i,j}$  can be written as:

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where:

$$\begin{aligned} U_{ij} &= (\left| a2_{i+1,j} - a1_{i+1,j} \right| + w) / (\left| b2_{i,j} - b1_{i,j} \right| + w) \\ V_{ij} &= (\left| a2_{i,j+1} - a1_{i,j+1} \right| + w) / (\left| c2_{i,j} - c1_{i,j} \right| + w) \end{aligned}$$

and the empirical parameter w > 0 is necessary for correct division when differences  $(b2_{i,j} - b1_{i,j})$ ,  $(c2_{i,j} - c1_{i,j})$  are close to noises value d.

If all  $g_{i,j}$  are determined then the system of equations for  $f_{i,j}=(h_{i,j}/g_{i,j})$  can be received from first (K=1) or last (K=2) part of (4) and written as:

where:

$$\begin{aligned} q_{i,j} &= \left(a \mathcal{1}_{i+1,j} / g_{i+1,j}\right) \cdot \left(b \mathcal{1}_{i,j} / g_{i,j}\right) \\ p_{i,j} &= \left(a \mathcal{1}_{i,j+1} / g_{i,j+1}\right) \cdot \left(c \mathcal{1}_{i,j} / g_{i,j}\right) \end{aligned}$$

are known values.

Digital correction of any image  $\{a_{i,j}\}$  for arbitrary G and H come to be according to expressions:

$$I_{i,j} = G.(a_{i,j} \mid g_{i,j}) - (f_{i,j} + H) \qquad 1 \le i,j \le N$$
 (7)

Overdetermined non-correct systems of linear equations (5) and (6) in principle can be solved by well known least squares method. According to theoretical estimates [18] this method permits to restore  $\{l_{i,j}\}$  with accuracy:

$$D \approx (\ln N)^{1/2} \cdot d \tag{8}$$

close to detectors' noise d practically for any N. But its numerical realization encounters some problems because of large operations' number (from  $\approx N^4$  to  $\approx N^3 - N^{5/2}$  for best iterative methods) and principal limitation on computer accuracy [18 and 19].

We have developed non-iterative hierarchical method for solution systems (5) and (6) which are matched by accuracy the detectors' noise and require only  $\approx 100 \ N^2$  arithmetical operations for any N.

Equations of system (5) can be interpreted as recurrent expressions which permit to found any  $g_{i+k,j+l}$  (with k=0, 1 and l=0, 1), if  $g_{ij}$  are known. Because of 2D  $\{g_{ij}\}$  there are many ways for such a procedure and average with using some of neighbouring ones can be done. Thus if  $g_{1,1}=1$ , then first order approximation  $g_{12}^{(1)}$ ,  $g_{21}^{(1)}$ ,  $g_{13}^{(1)}$ ,  $g_{22}^{(1)}$ ,  $g_{31}^{(1)}$ ,...  $g_{NN}^{(1)}$ , can be obtained and new recurrent expressions for next order approximation  $\{g_{ij}^{(2)}\}$  can be written. This procedure is repeated  $m \leq [\ln N] - 2$  times with using every one more large-scale nets [N/2]. [N/2], [N/4],... $[N/2^m]$ .  $[N/2^m]$  and more large detectors' blocks (2.2), (4.4)...  $(2^m.2^m)$  considered as one element, respectively. Consideration for system (6) is the same.

It is important that in conveyor regime the algorithms could be reduced up to  $N^2$  operations.

Practical realization of the algorithms has been done by using IBM-PC/AT for

N < 256. Results of numerical simulation agree with theoretical estimate (8) and some of them for N = 128 and case when  $h_{i,j} = 0$  are demonstrated on figure 1.

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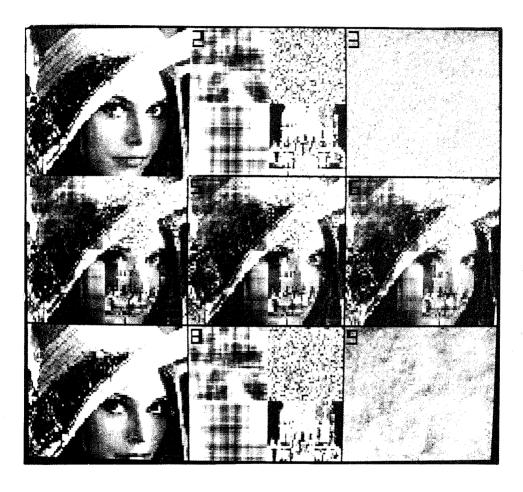


Fig.1. - Results of numerical simulation: (1,2) correspond to test images  $\{l_{i,j}\}$   $(l_{min}=65, l_{max}=216)$ ,  $\{g_{i,j}\}$   $(g_{min}=0.54, g_{max}=1.50)$ ; (3) is an example of detectors' noise  $\{d_{i,j}\}$   $(< d_{i,j}>=0, < d_{i,j}>=1)$  amplified by factor 8; (4-6) are the results of simulation for direct problem and correspond to  $\{a_{i,j}\}$ ,  $\{b_{i,j}\}$ ,  $\{c_{i,j}\}$  with independent additive detectors' noises; (7,8) are images  $\{l'_{i,j}\}$ .  $\{g'_{i,j}\}$  restored from (4-6) and (9) is difference between  $\{l_{i,j}\}$  and  $\{l'_{i,j}\}$  multiplied by factor 8.