1. Introduction

The geometrical (spatial) resolution is defined as the thermograph ability to reproduce the geometrical details in the thermal image. There are many ways in literature to define the geometric resolution of the thermal imaging systems [1], [2], [3], [4]. Sometimes makes it difficult to compare the metrological features of these devices carried to determine their ability to distinguish in the thermal images of tested objects their geometric details. The paper presents some of the most common ways to define this parameter and the method of comparing their values.

2. Methods of defining the geometric resolution of IR thermograph

In technical and scientific articles are used a number of different ways of defining geometric resolution of the thermographs. Here are a few of these definitions. 1) The geometric resolution is determined by the angular size of the active detector area (pixel) transferred to the object space of the camera optical system (GR1). 2) The geometric resolution is defined as the angle at which the camera "sees" a single flat object with the width of the vertical at which the maximum value of the measurement signal is 50% of the signal corresponding to the temperature of the large object (GR2) [3], fig. 1 and fig 2. It is assumed that all points of this object have the same temperature. Using the function of SRF (Slit Response Function) GR2 can be defined as such an argument value of SFR for which a value to this function is 0.5.

Fig. 1 Methods of measuring the geometrical resolution according to 2 definition
3) The geometric resolution is determined as that angular width at which the line spread function (LSF) of the thermograph has dropped to 40% (GR3) [2], fig. 3 and fig 4. 4) The geometric resolution is determined as that half the inverse of spatial frequency at which the modulation transfer function (MTF) of the thermograph has dropped to 50% (GR4) [1].

3. Comparison of geometric resolution defined by various methods

It is easy to see that the definition of 1 cannot be compared with the definitions 2-4. This is because it combines the geometric resolution of the thermograph only with the parameters describing the geometry of the optical system. It does not take into account in this case, the impact of optical aberrations, detector time constant and filtration of the electronic circuit. Comparative analysis of definition of 2-4 will be referenced to a class thermographic...
devices that filter characteristics can be described using the theory of linear filtering. Based on literature data it was assumed that, for thermograph properly designed and constructed, the LSF function can be approximated by a Gaussian function:

\[ LSF(\alpha) = \exp \left( -\frac{\alpha^2}{\sigma^2} \right) \]  \hspace{1cm} (1)

where: \( \alpha \) - angular coordinate, \( \sigma \) – a constant value, expressed in angular units.

According to the definition 2, geometric resolution \( GR_2 \) of the thermograph can be determined by calculating the value of the angle \( \alpha_0 \) for which the equation (2) is fulfilled:

\[ \frac{\int_{-\pi/2}^{\pi/2} LSF(\alpha) d\alpha}{\int_{-\infty}^{\infty} LSF(\alpha) d\alpha} = \frac{1}{2} \]  \hspace{1cm} (2)

where: \( \alpha_0 \) - angular coordinate value.

Thus, in accordance with the definition 2, \( GR_2 = \alpha_0 \). According to the definition 4, geometric resolution \( GR_4 \) resolution can be obtained by determination of such a value of spatial frequency \( f_{pa} \) defined in the image plane, for which the equation (3) is fulfilled:

\[ MTF(f_{pa}) = 1/2 \]  \hspace{1cm} (3)

Thus:

\[ GR_4 = 1/2 f_{pa} \]  \hspace{1cm} (4)

Taking into account that:

\[ MTF(f_{pa}) = \frac{\left| \int_{-\infty}^{\infty} LSF(\alpha)e^{-j2\pi f_{pa}\alpha} d\alpha \right|}{\int_{-\infty}^{\infty} |LSF(\alpha)| d\alpha} \]  \hspace{1cm} (5)

as well as considering that LSF function can be approximated by a Gaussian function, then from formulas (1) and (5) we obtain:

\[ MTF(f_{pa}) = \exp (-\pi^2 \sigma^2 f_{pa}^2) \]  \hspace{1cm} (6)
After taking into account relations (3) and (6) we get:

$$GR4 = \frac{\pi \sigma}{2 \sqrt{\ln 2}} \approx 1.88\sigma.$$  \hspace{1cm} (7)

In a similar manner as above can be shown that:

$$GR3 = 2\sqrt{\ln 10/\ln 2} \sigma \approx 1.91\sigma,$$ \hspace{1cm} (8)

and that

$$GR2 \approx 0.96\sigma.$$ \hspace{1cm} (9)

4. Summary

It is possible to convert the geometric resolution values defined in various ways. It is not possible to do this only in the case of the definition, which combines the geometric resolution of the thermograph only with the parameters describing the geometry of the optical system.

REFERENCES